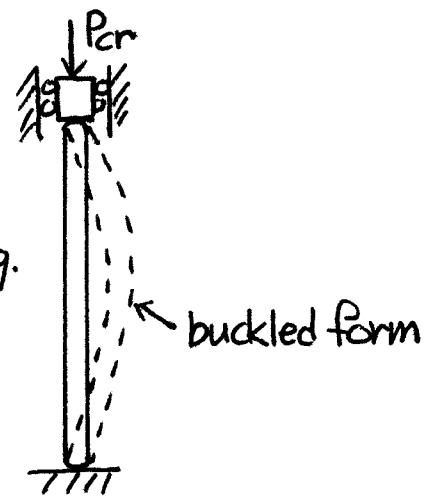
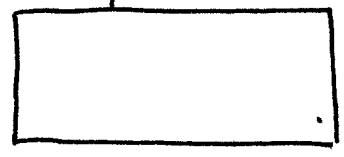


# CH12. COLUMN BUCKLING

## 12.1. Introduction

- Straight column with pin joints fails with compressive load  $P_{cr}$  by elastic buckling.



- $P < P_c$ , small lateral force, or eccentricity of  $P$ , provides stable elastic response.
- $P > P_c$ , small lateral force causes large deflection and eventually fracture.

## 12.2. Deflection of a Column

### 1. Ideal Slender Column

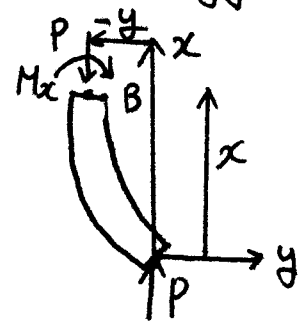
- pin jointed column

$I = A r^2$  ↗ radius of gyration

## 12.3. Euler Formula for Pin Joints

~ Equilibrium method, imperfection method, energy method.

### 1. Equilibrium Method



Curvature  $K = \frac{1}{R} = \frac{M_x}{EI}$   $R$ : radius of curvature

$$M_x =$$

$$\Rightarrow M_x = EI \frac{d^2 y}{dx^2} = -Py$$



where  $k^2 = \frac{P}{EI}$

column buckling differential eq.

similar to vibration prob.

Boundary conditions

$$y = 0 \text{ at } x = 0, x = L.$$

General Solution

$$y(x) = A \sin kx + B \cos kx$$

$$y(0) = B = 0$$

$$y(L) = A \sin kL = 0, \sin kL = 0, kL = n\pi$$

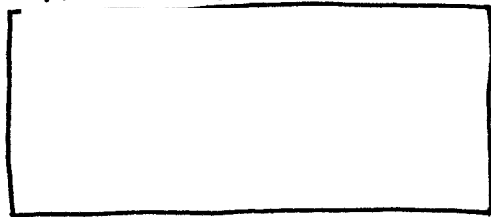
$$k = \sqrt{\frac{P}{EI}} = \frac{n\pi}{L} \quad n = 1, 2, 3, \dots$$

$$\therefore y(x) =$$

Corresponding Euler load

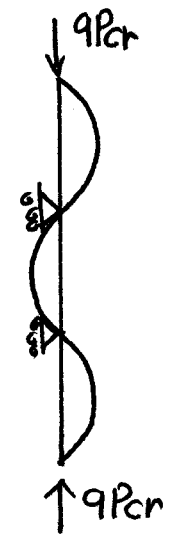
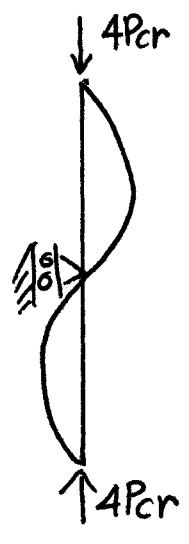
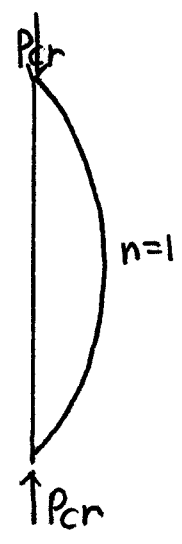
$$P =$$

$n=1 \Rightarrow$  minimum load  $\Rightarrow$  critical load



$A_1$  cannot be determined in this approach.

## 2. Higher Buckling Loads; $n > 1$



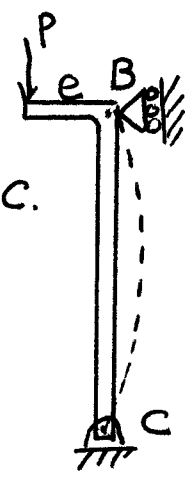
- When the column is prevented from  $P_{cr}$  load by fixing center location, then it buckles with  $n=2$ .

For any  $n$  :

$$P =$$

## 3. Imperfection Method

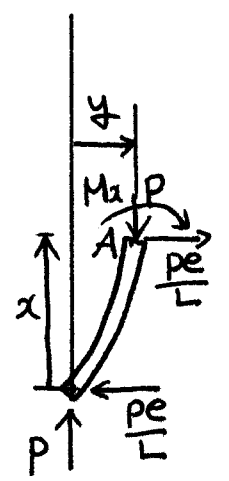
- From moment equilibrium at B there must be a horizontal force at C.



- From the moment equilibrium at A

$$\sum M_A = M_x + \frac{Pex}{L} + py = 0$$

=>



Differential Eq.

$$\frac{d^2y}{dx^2} + \frac{P}{EI} y = -\frac{Pe x}{EIL}$$

Let  $k = \sqrt{\frac{P}{EI}}$



Boundary condition

$$y(x) = 0 \text{ at } x=0, x=L$$

General Solution

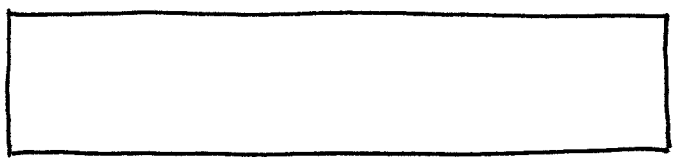
$$y(x) = A \sin kx + B \cos kx - \frac{ex}{L}$$

$$y(0) = B - \frac{ex}{L} = 0 \quad B = 0$$

$$y(L) = A \sin kL + B \cos kL - e = 0$$

$$A = \frac{e}{\sin kL}$$

$$\therefore y(x) =$$



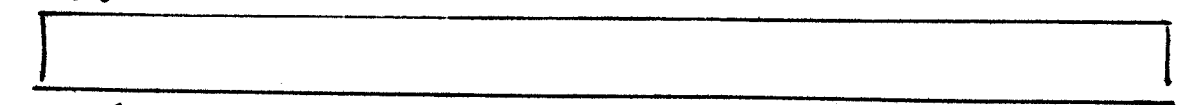
Displacement  $y \rightarrow \infty$  when

$$kL = n\pi. \text{ when } n=1$$

$$P = P_{cr} = \frac{\pi^2 EI}{L^2}$$

4. Energy Method

Energy conservation



↑  
work done  
by external  
force

↑  
Heat energy  
input

↑  
increase in  
strain energy

↑  
increase in  
kinetic energy

# Application to Column Buckling

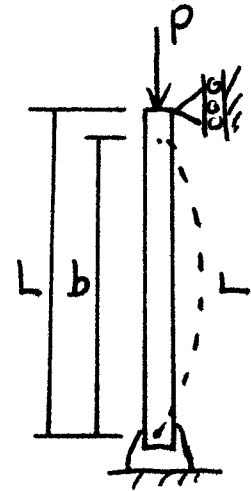
- infinitesimal motion :  $\delta K \ll \delta U, \delta W,$
- adiabatic :  $\delta H = 0$

$\Rightarrow$

It is assumed that the column may buckle when the load first reaches a value for which  $\delta W = \delta U$

Fourier series expansion

: satisfy B.C.  $y=0$  at  $0, L.$



Strain energy resulting from bending

$U_M =$

$$U_M = \int \frac{M^2}{2EI} dx \quad M = EI y''$$

$$y'' = -\sum_{n=1}^{\infty} \left(\frac{n\pi}{L}\right)^2 a_n \sin \frac{n\pi x}{L}$$

$$\int_0^L \sin \frac{m\pi x}{L} \sin \frac{n\pi x}{L} dx = \begin{cases} 0 & m \neq n \\ \frac{L}{2} & m = n \end{cases}$$

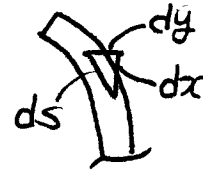
$\Rightarrow U_M = \frac{1}{2} EI \sum_{n=1}^{\infty} \left(\frac{n\pi}{L}\right)^4 a_n^2 \cdot \frac{L}{2}$

$U_M =$

- Bar will buckle without changing its length  $L$ .

$$ds^2 = dx^2 + dy^2$$

$$= dx^2 \left( 1 + \left( \frac{dy}{dx} \right)^2 \right)$$



$$ds = \sqrt{1 + (y')^2} dx$$

$$L = \int_0^b \sqrt{1 + (y')^2} dx$$

binomial expansion

$$\sqrt{1 + (y')^2} = 1 + \frac{1}{2}(y')^2 + \text{H.O.T.}$$

$$L \approx \int_0^b \left[ 1 + \frac{1}{2}(y')^2 \right] dx$$

$$= b + \int_0^b \frac{1}{2}(y')^2 dx$$

$$\therefore L - b \approx$$

- Work done by force  $P$

$$\delta W = P(L - b) = \frac{P}{2} \int_0^L (y')^2 dx.$$

$$y' = \sum_{n=1}^{\infty} \frac{n\pi}{L} a_n \cos \frac{n\pi x}{L}$$

$$\delta W = \sum_{n=1}^{\infty} \frac{P}{2} \cdot \left( \frac{n\pi}{L} \right)^2 a_n^2 \cdot \frac{L}{2}$$



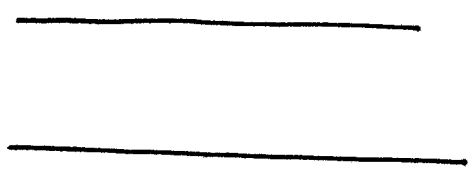
$$\delta W = \delta U$$

$$\frac{\pi^2 P}{4L} \sum_{n=1}^{\infty} n^2 a_n^2 = \frac{\pi^4 EI}{4L^3} \sum_{n=1}^{\infty} n^4 a_n^2$$



• If  $a_1 \neq 0$  &  $a_2 = a_3 = \dots = 0$

=>



• If  $a_2 \neq 0$ ,  $a_1 = a_3 = a_4 = \dots = 0$

$P =$  : second buckling load.

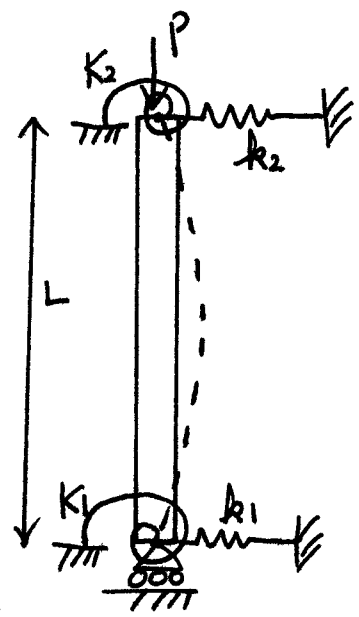
12.4. Euler Buckling with Elastic Constraint

• Potential Energy

$V =$

+

+



• Stationary condition of V

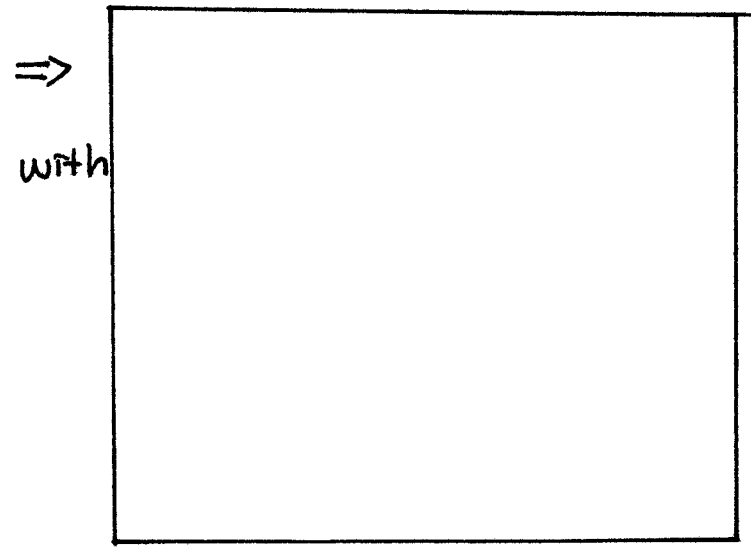
$$\delta V = K_2 y_2' \delta y_2' + k_2 y_2 \delta y_2 + K_1 y_1' \delta y_1' + k_1 y_1 \delta y_1 + EI \int_0^L \underbrace{y'''}_{u} \delta \underbrace{y''}_{v} dx - P \int_0^L \underbrace{y'}_{u} \delta \underbrace{y'}_{v} dx = 0.$$

• Integration by Parts

$$\Rightarrow (K_2 y_2' + EI y_2''') \delta y_2' + (K_1 y_1' - EI y_1''') \delta y_1' + (k_2 y_2 - P y_1') \delta y_2 + (k_1 y_1 + P y_1') \delta y_1 - EI \int_0^L y_2'''' \delta y_2' dx + P \int_0^L y_1'''' \delta y_1 dx = 0$$

• Integration by Parts

$$(K_2 y_2' + EI y_2'') \delta y_2' + (K_1 y_1' - EI y_1'') \delta y_1' + (k_2 y_2 - P y_2' - EI y_2''') \delta y_2 + (k_1 y_1 + P y_1' + EI y_1''') \delta y_1 + EI \int_0^L y'''' \delta y dx + P \int_0^L y'' \delta y dx = 0.$$



- 1 → x = 0
- 2 → x = L

Euler equation for column

• General solution

y =

k = P/EI.

For general case, substitute y into 4 B.C.s

$$\left[ \begin{matrix} \Delta \\ \Delta \\ \Delta \\ \Delta \end{matrix} \right] \begin{matrix} A \\ B \\ C \\ D \end{matrix} = 0 \Rightarrow |\Delta| = 0 \text{ will lead to the critical load condition}$$

• Specific B.C.s

pinned ends :  $y_1 = 0 \quad y_2 = 0 \quad , \quad \delta y_1 = \delta y_2 = 0$   
 $K_1 = K_2 = 0$

B.C. ⇒  $\begin{cases} y_1'' = 0 \\ y_2'' = 0 \end{cases}$

$B = C = D = 0.$        $A \sin kL = 0 \quad kL = n\pi \quad P_{cr} = \frac{\pi^2 EI}{L^2}$



Example 12.1. Clamp-Free Column

Clamped one end ( $x=0$ ) & free ( $x=L$ ).

$$y_1 = 0, \quad y_1' = 0, \quad \delta y_1 = \delta y_1' = 0$$

$$K_2 = k_2 = 0 \quad (\text{free end})$$

B.C. (

$$y_1 = 0; \quad B + D = 0, \quad y_1' = 0; \quad kA + C = 0$$

$$y_2'' = 0; \quad A \sin kL + B \cos kL = 0,$$

$$EI y_2'' + P y_2' = 0; \quad y_2'' + k^2 y_2' = 0 \Rightarrow C = 0$$

$$\therefore A = C = 0, \quad B = -D, \quad \cos kL = 0$$

$$\therefore kL = \frac{(2n-1)\pi}{2} \quad n=1 \quad kL = \frac{\pi}{2}$$

$$\therefore P =$$

12.5. Local Buckling

~ Local buckling of flange or web before it fails as an Euler Beam.

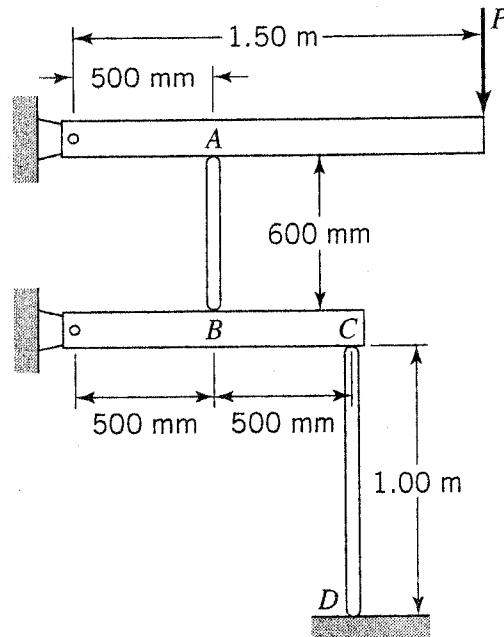
~  $\frac{t}{b}$  large, buckle as an Euler column

$\frac{t}{b}$  small, local buckle, sheet buckling, plate buckling wrinkling

~ Local buckling may not cause immediate collapse.

It alters stress distribution, reduces compressive stiffness

12.8. In Figure P12.8, columns  $AB$  and  $CD$  have pinned ends, are made of an aluminum alloy ( $E = 72.0$  GPa), and have equal rectangular cross sections of 20 mm by 30 mm. Determine the magnitude of  $P$  that will first cause one of the columns to buckle. Assume elastic conditions.



**FIGURE P12.8**

12.12. Determine the Euler load for the column shown in Figure 12.8c; see the discussion on the imperfection method in Section 12.3.